

Post-EPS Scatterometer Performance Simulation

[Ad.Stoffelen @knmi.nl](mailto:Ad.Stoffelen@knmi.nl)

Maria Belmonte, UCAR

Jos de Kloe, KNMI

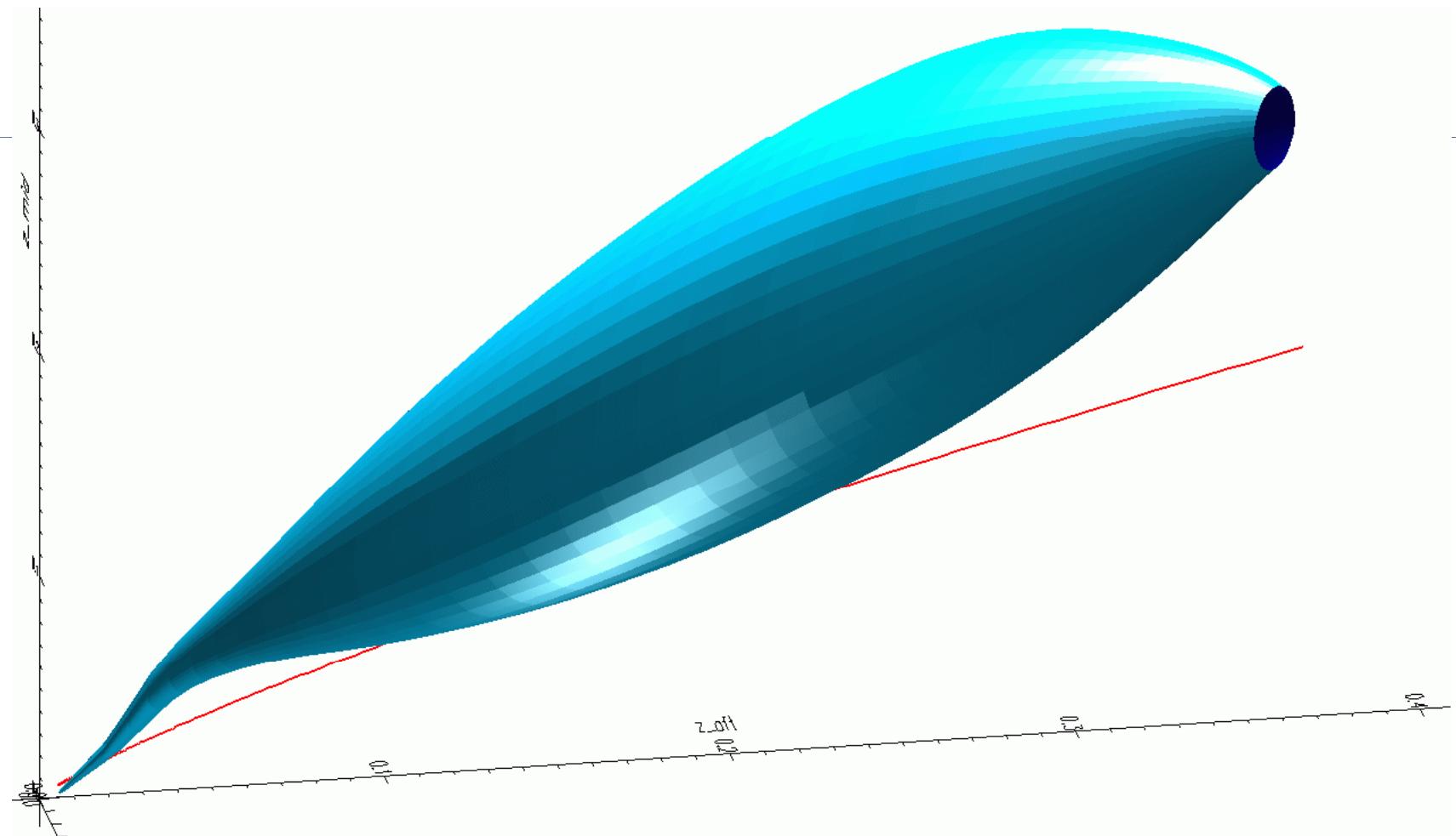
ESA Study



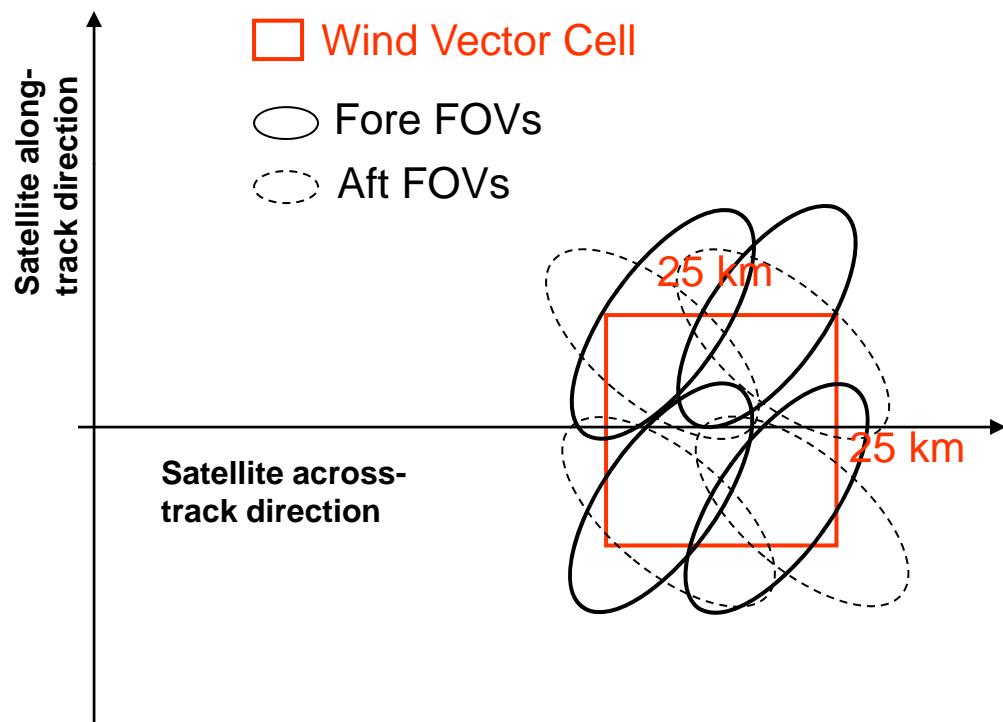
IOVWST, May 2010

Wind retrieval and noise model

- ✓ Kp noise
- ✓ Geophysical noise due to ocean variability
- ✓ Approximate retrieval functions



Geophysical noise



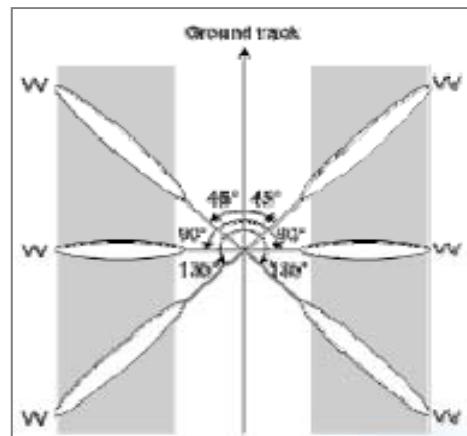
Post EPS scatterometer (SCA)

[baseline requirements and options]

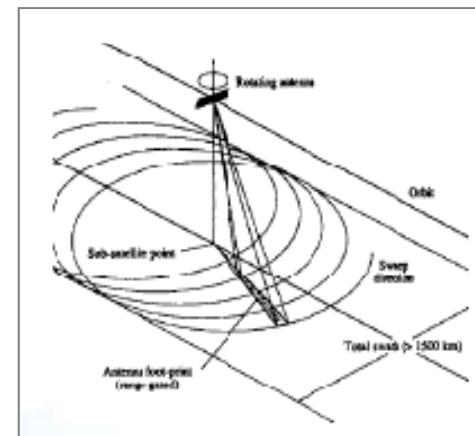
- Spatial resolution (25 km)
- Dynamic range (4-25 m/s)
- Radiometric resolution (~3-10% at 4 m/s)
- Swath coverage (95% in 48 hours for incidences between **20** and **60°**)
15% improvement with respect to ASCAT on MetOp

MetOp orbit → Sun Sync
with 820 km altitude

I - Fixed beam (ASCAT type)



II - Rotating beam (RFSCAT type)



Discarded: Ku-band (rain), pencil beam (skill), extended nadir coverage for ASCAT type

Specify complete SCA arrangement:

1) Antenna configuration

(C-band, single vs dual pol):

- total power
- dimensions
- radiation pattern

2) Radar waveform

(FM chirp, short vs long pulse):

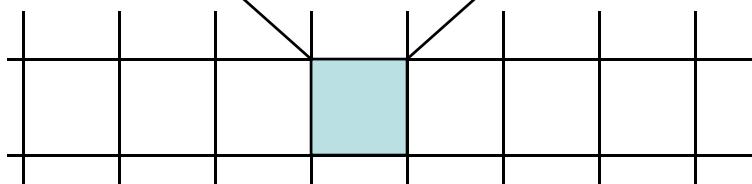
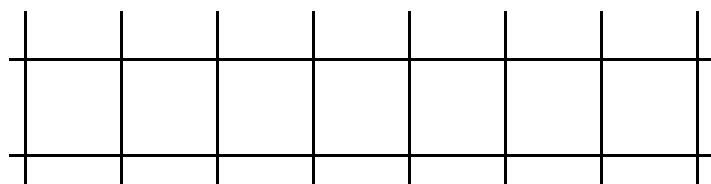
- PRF
- chirp bandwidth
- noise estimation

Orbital model

Pseudo Level 1B file

Incidence / Azimuth
Polarization
NESZ
 N_{looks}
 N_{noise}

views



Satellite
position
at time t

WVC

(25 km resolution cell)

Radiometric resolution (NESZ and K_p)

1) NESZ (Noise Equivalent Sigma Zero) for a single look:

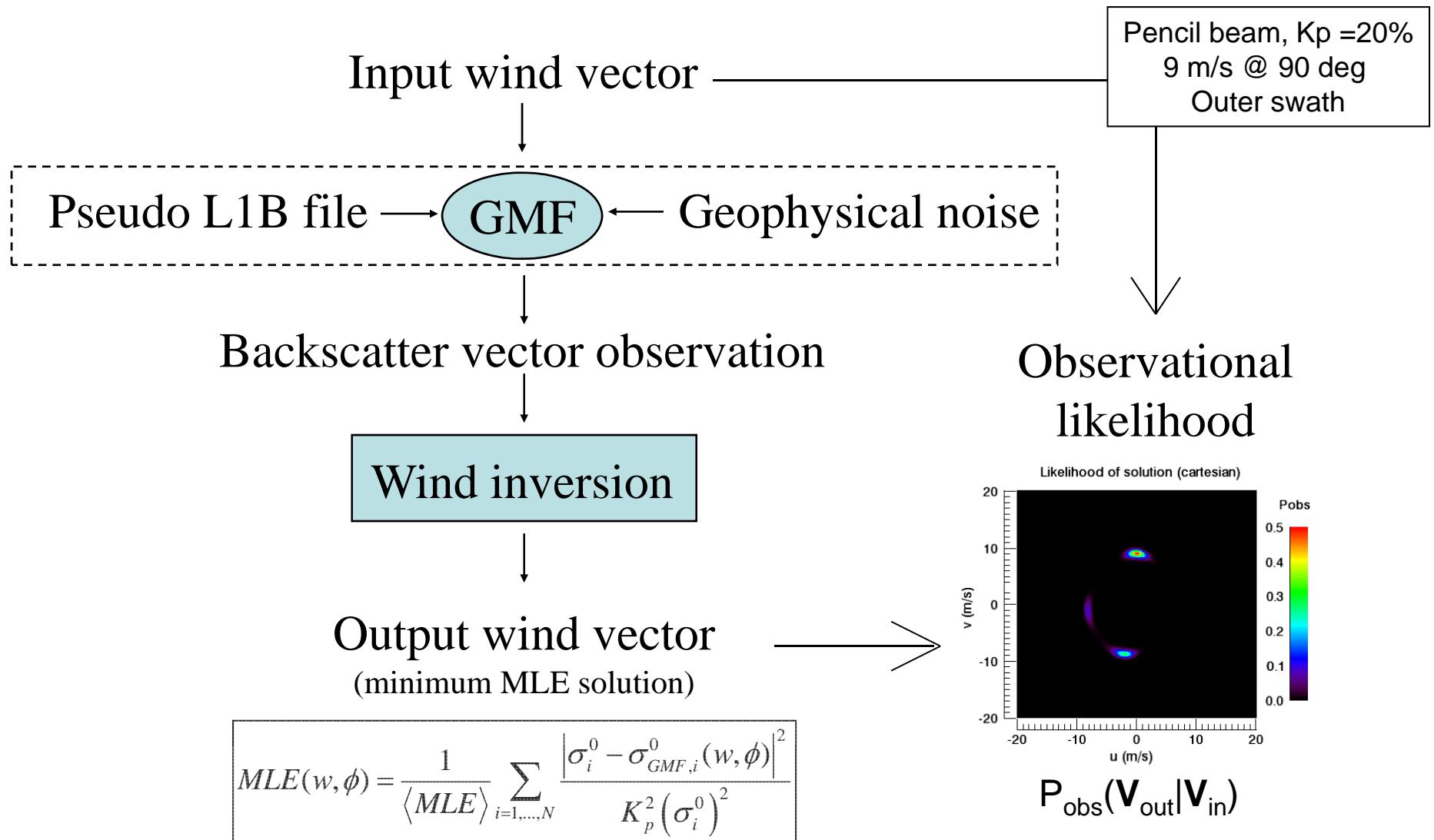
$$NESZ = \frac{\sigma^0}{SNR} = \frac{k_B(T_0 + T_{eq})}{\frac{\lambda^2}{(4\pi)^3} \left(\frac{P_t G_{TX} G_{RX}}{R^4 \cdot L_{prop}} \right)} \frac{B_{look}}{A_{look}} \quad A_{look} = \Delta_{range} \Delta_{azimuth}$$

2) Number of looks per node: $N_{looks} = \frac{\Delta x \Delta y}{A_{look}}$ (reduce speckle)

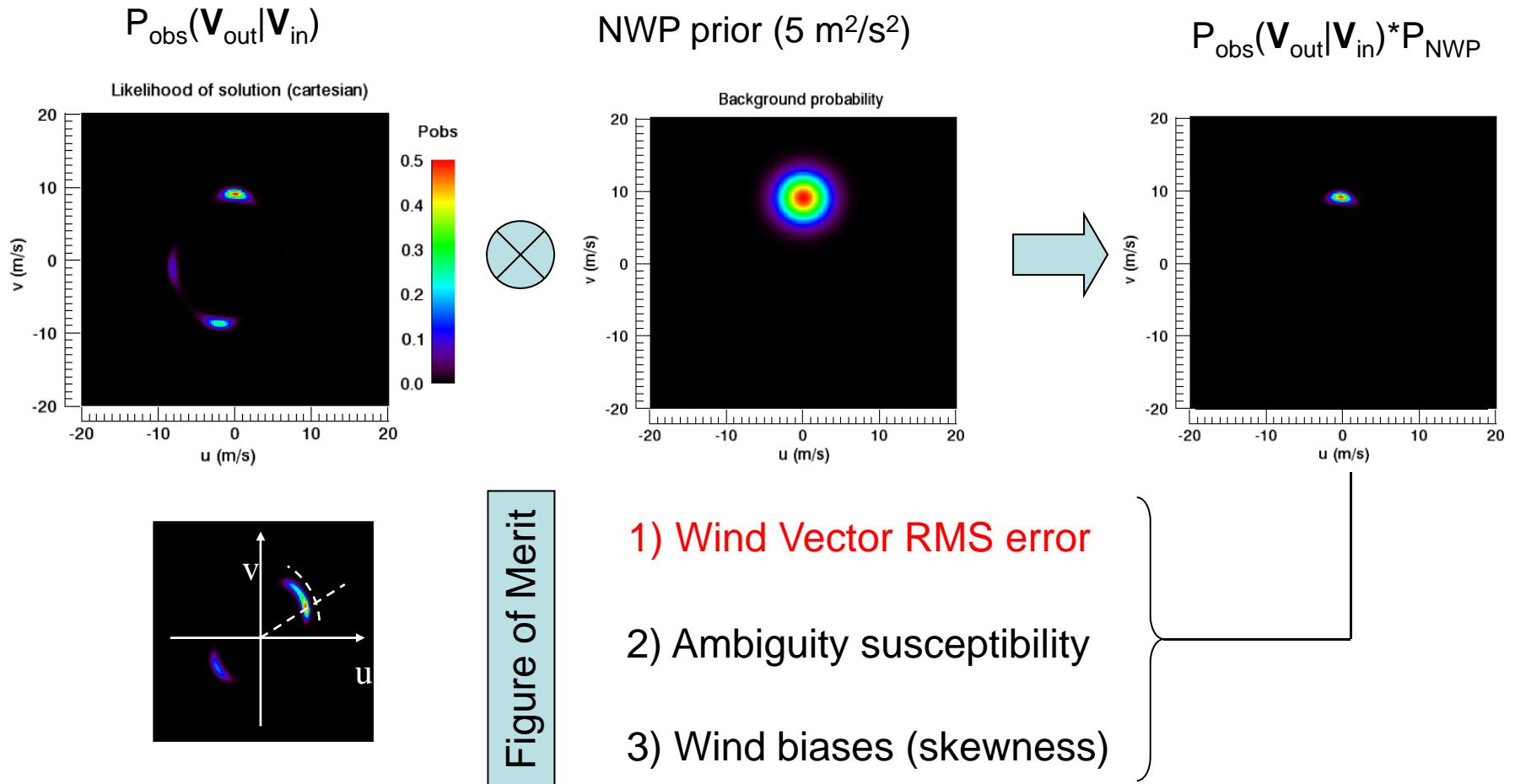
3) Number of noise samples: $N_{noise} = f_s T_{noise}$ (noise estimation)

Radiometric resolution: $K_p^2 = \frac{\text{var}\{\sigma^0\}}{\langle \sigma^0 \rangle^2} = \frac{1}{N_{looks}} \left(1 + \frac{1}{SNR} \right)^2 + \frac{1}{N_{noise}} \left(\frac{1}{SNR} \right)^2$

SCA end-to-end simulator



Wind retrieval performance

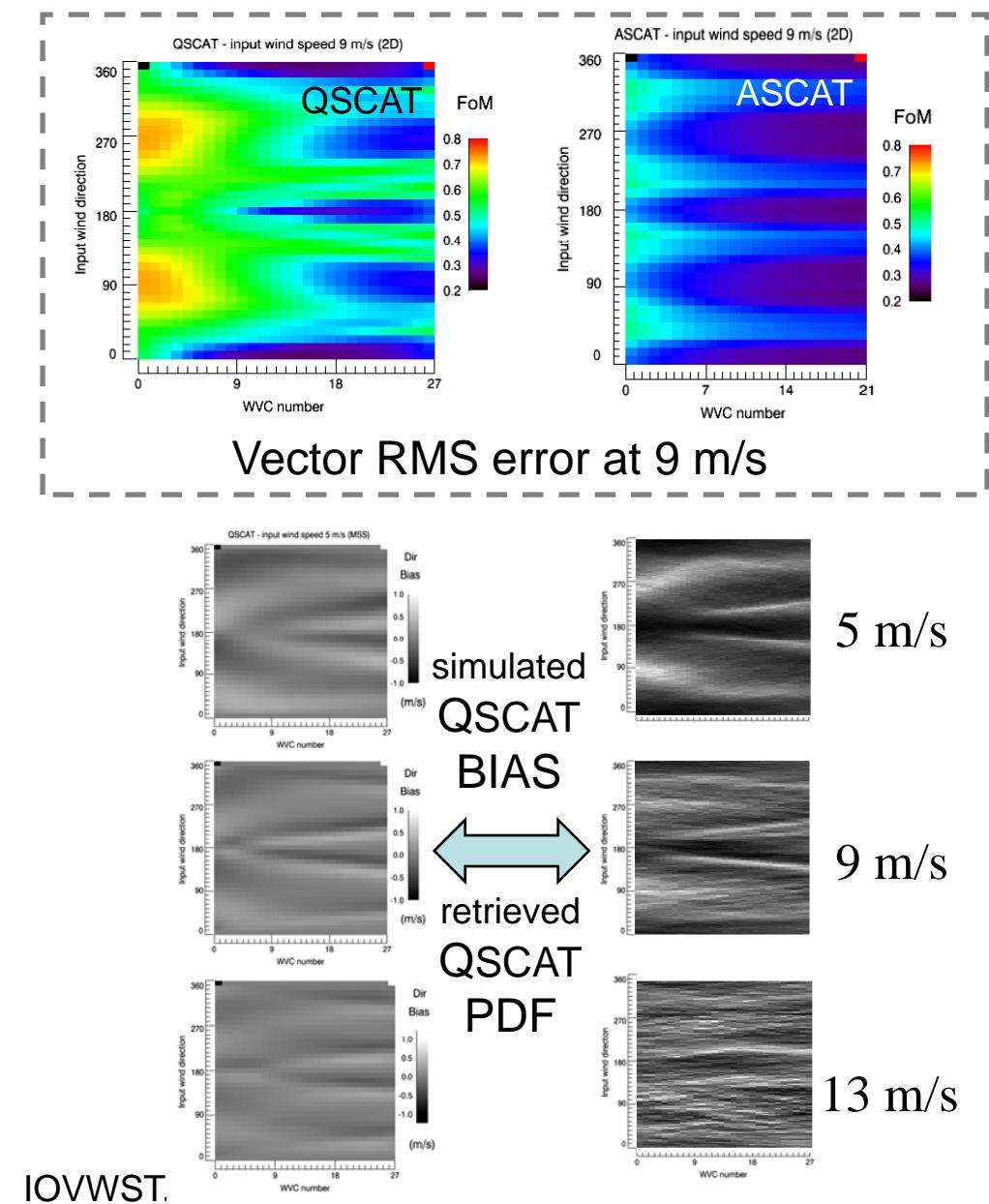
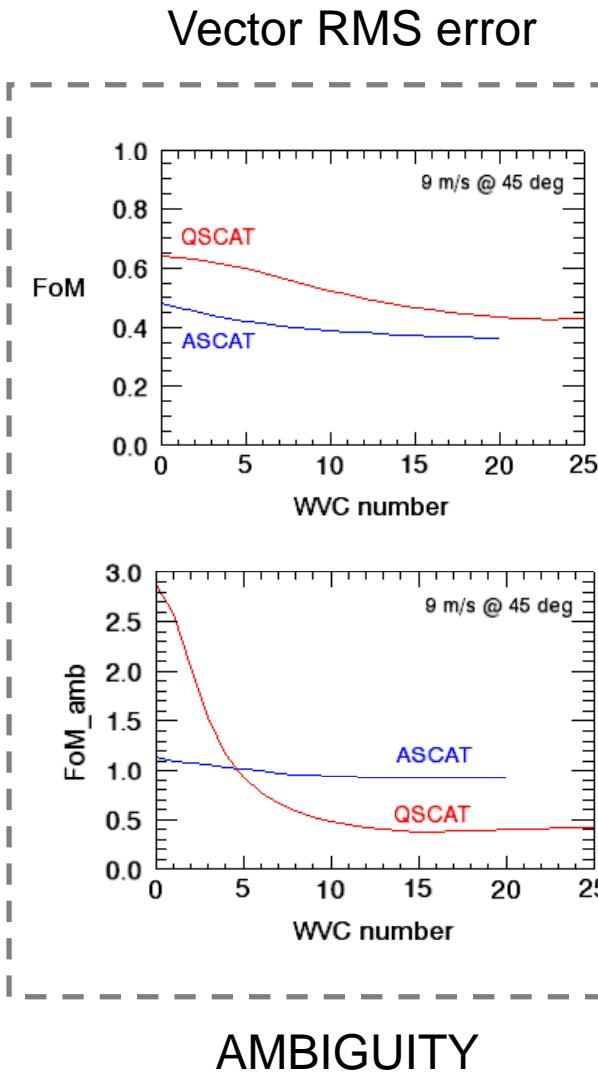


For example:

$$RMS_{\text{obs}}(\vec{v}_{\text{true}}) = \left(\int |\vec{v} - \vec{v}_{\text{true}}|^2 p_{\text{obs}}(\vec{v} | \vec{v}_{\text{true}}) p_{\text{bg}}(\vec{v}) d^2 v \right)^{1/2}$$

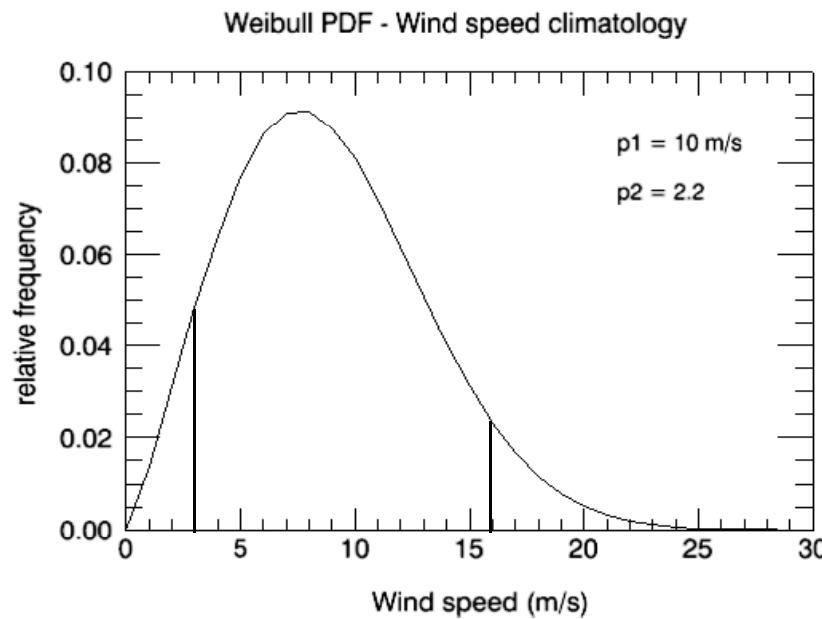
IOVWST, May 2010

Wind retrieval performance QSCAT/ASCAT



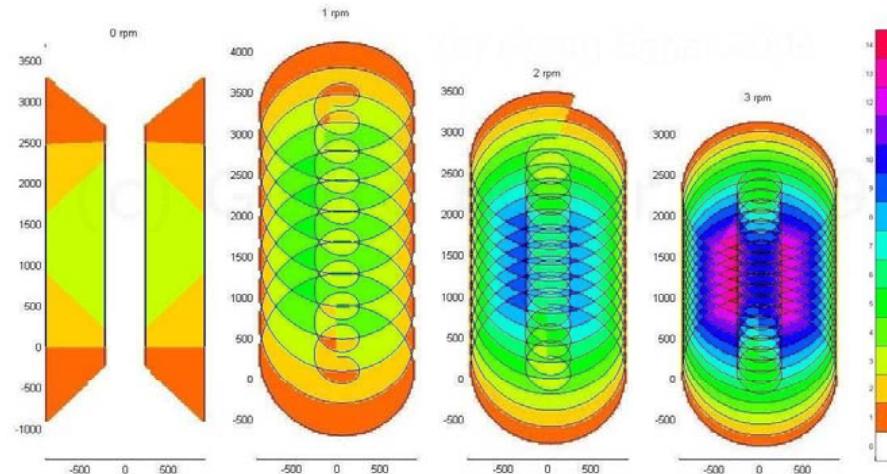
Climatology FoMs

Wind retrieval performance is dependent on input wind and across track distance



Use a climatology average over wind speeds (3-16 m/s)

SCA assessment

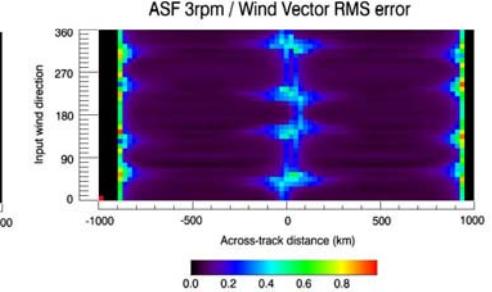
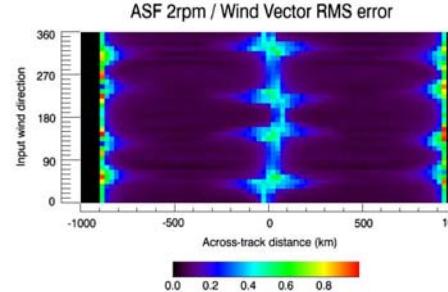
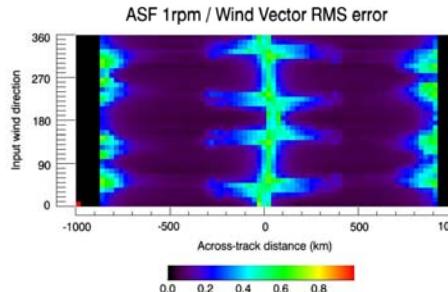
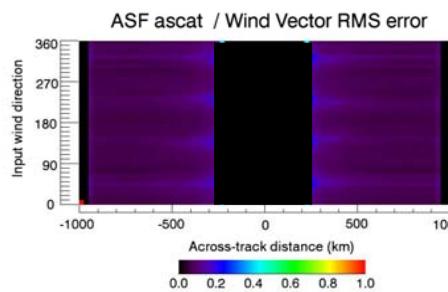


ASCAT
type

RFSCAT
(1rpm)

RFSCAT
(2rpm)

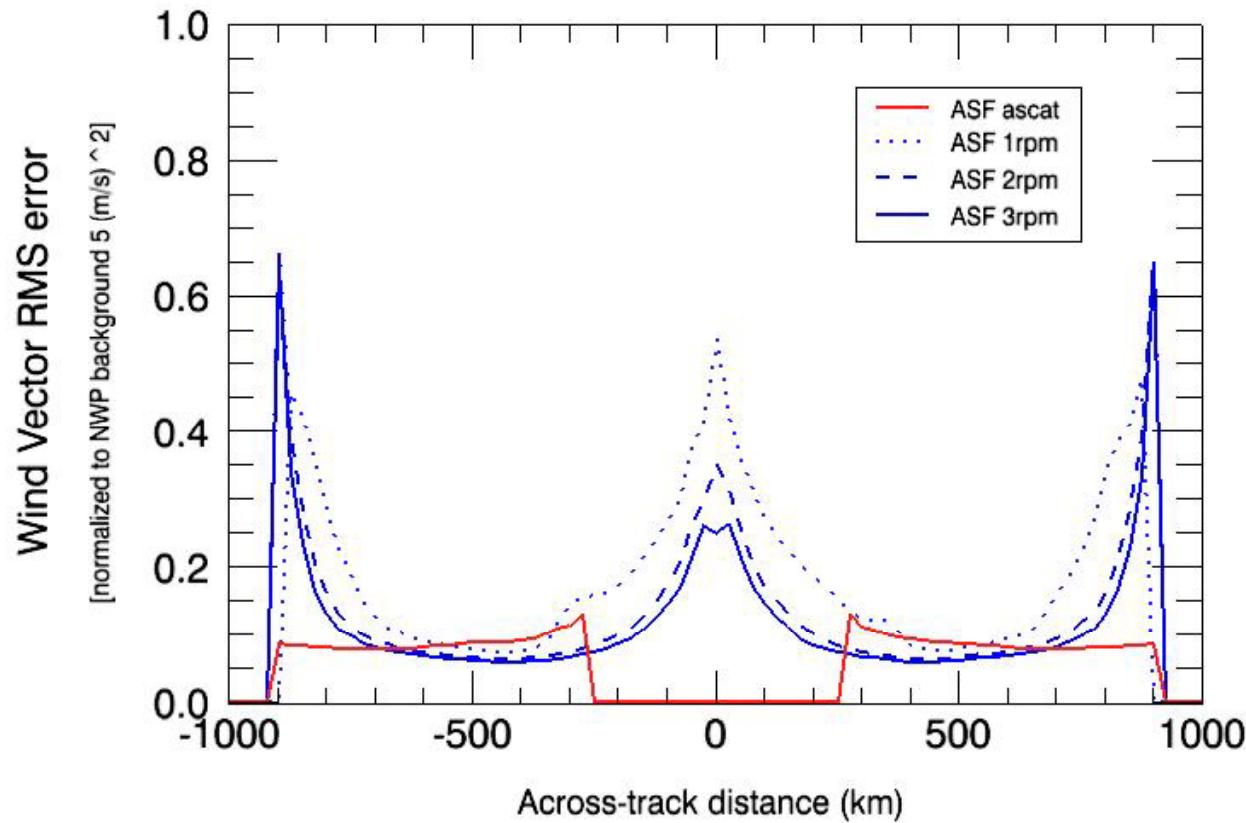
RFSCAT
(3rpm)



Wind Vector RMS error across swath
IOVWST, May 2010

Conclusion

RFSCAT performs well compared to ASCAT configuration, but ...



To consider: geophysical noise, HH polarization, resolution

To optimize: antenna pattern...
IOVWST, May 2010

Thank you !

scat@knmi.nl

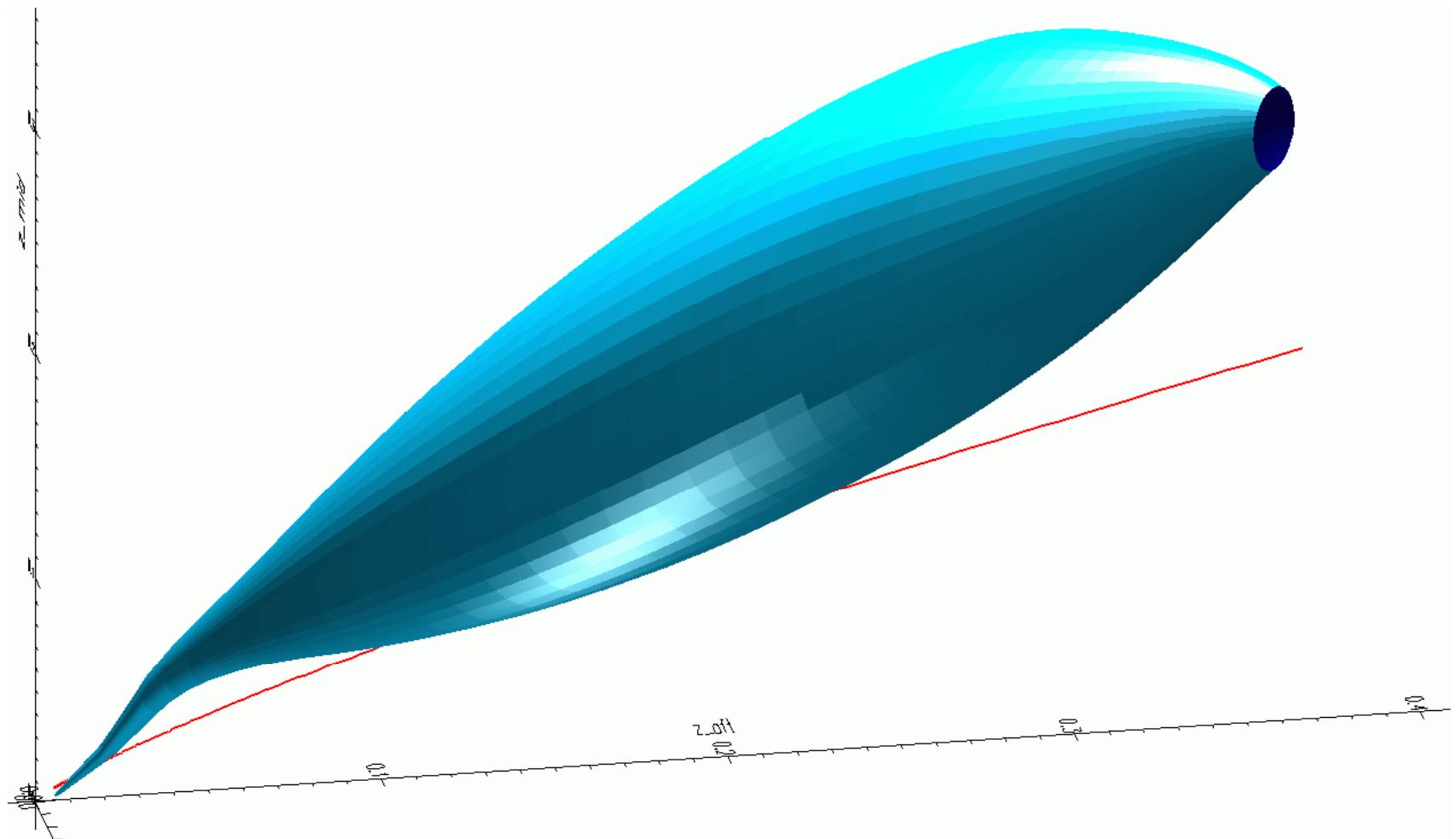
www.knmi.nl/scatterometer

Backup Slides

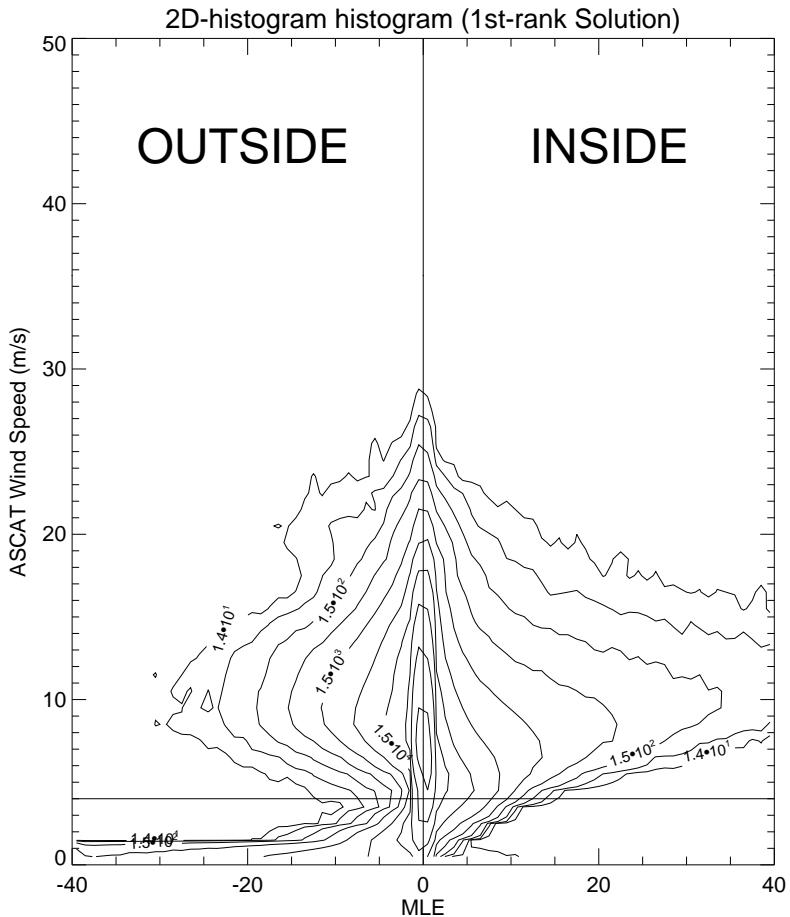
IOVWST, May 2010

Wind retrieval and noise model

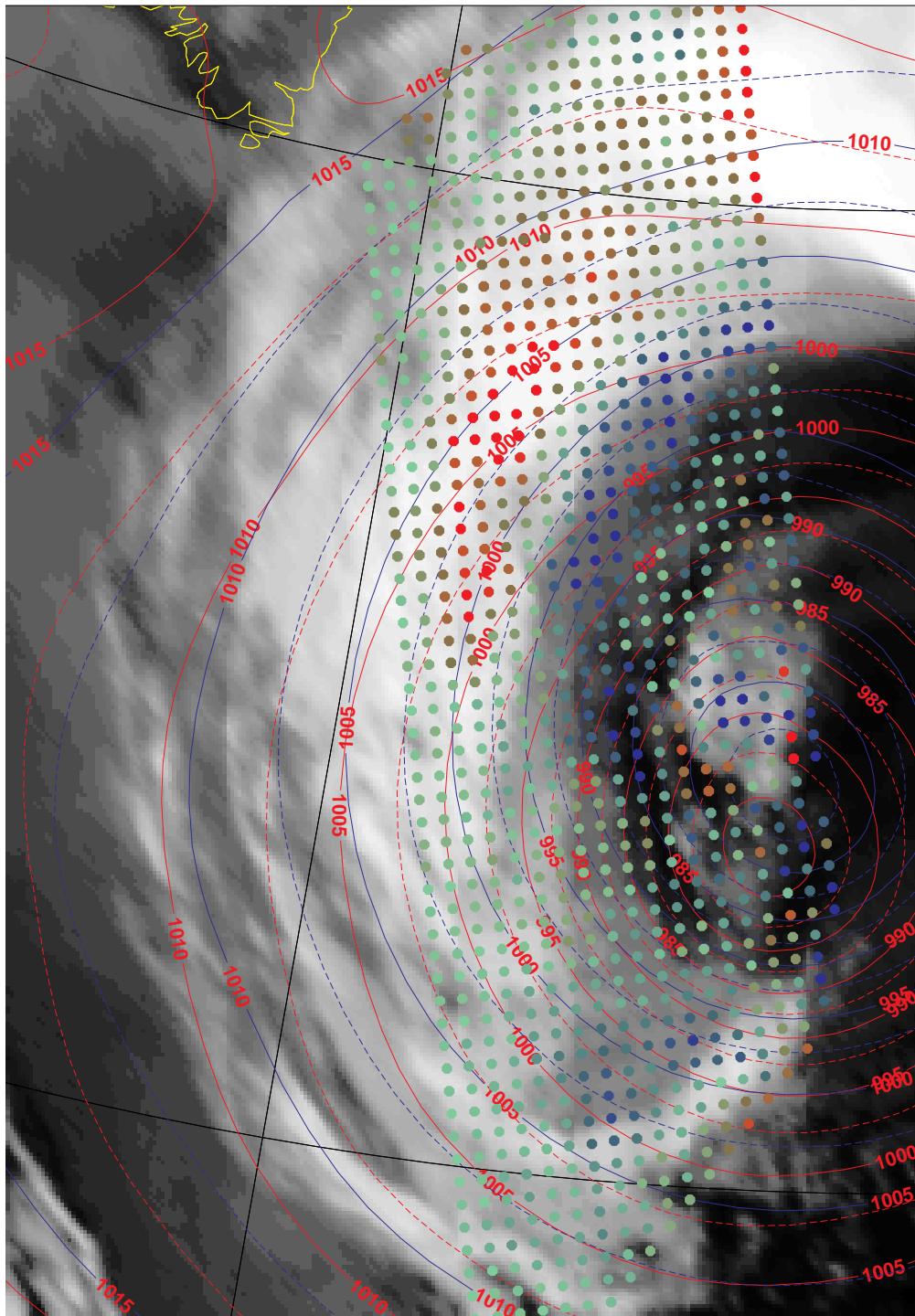
- ✓ Kp noise
- ✓ Geophysical noise due to ocean variability
- ✓ Approximate retrieval functions



GMF issues



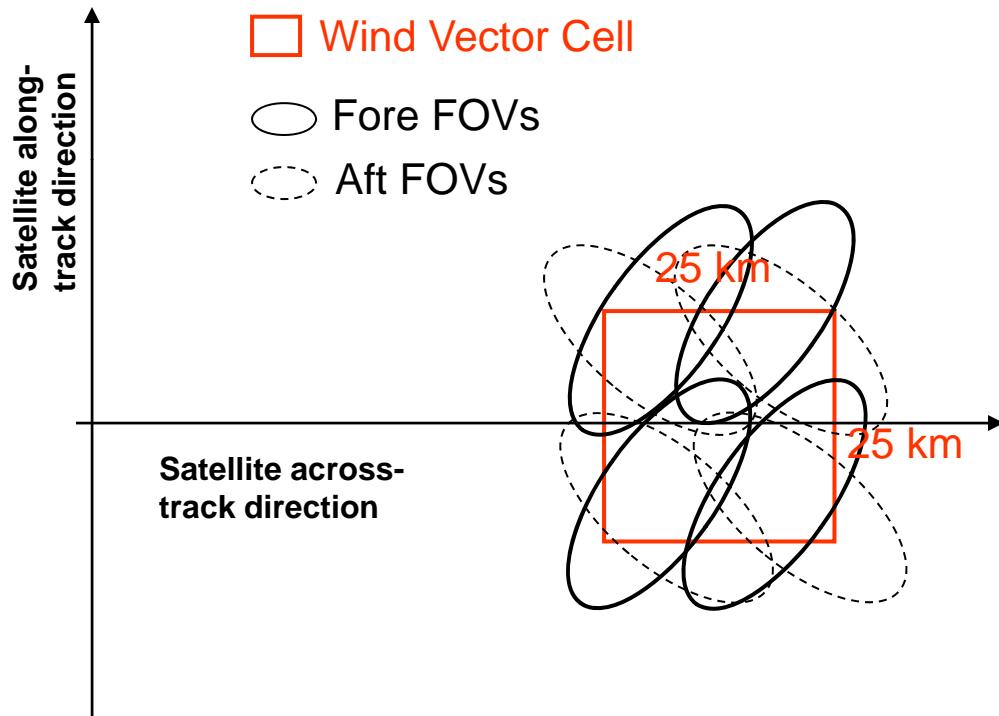
- Measured triplets are centered well on cone within Kp for all speeds
- Geophysical noise at low winds incorporated
- Reasonable symmetry at medium-high winds
- Around 4 m/s most triplets inside the cone
- At very low winds, opposite effect



ERS-2

- Warm steady-flow air discerned from polar gusty air.
- Wind variability causes triplet inconsistency
- Noise at edge of the swath; ASCAT moved outward

Geophysical noise



- Different kinds of FOVs are combined (views)
- Each WVC view represents a different areal mean
- The ocean surface is variable
- A geophysical error occurs due to ocean surface variability and WVC non-uniform sampling

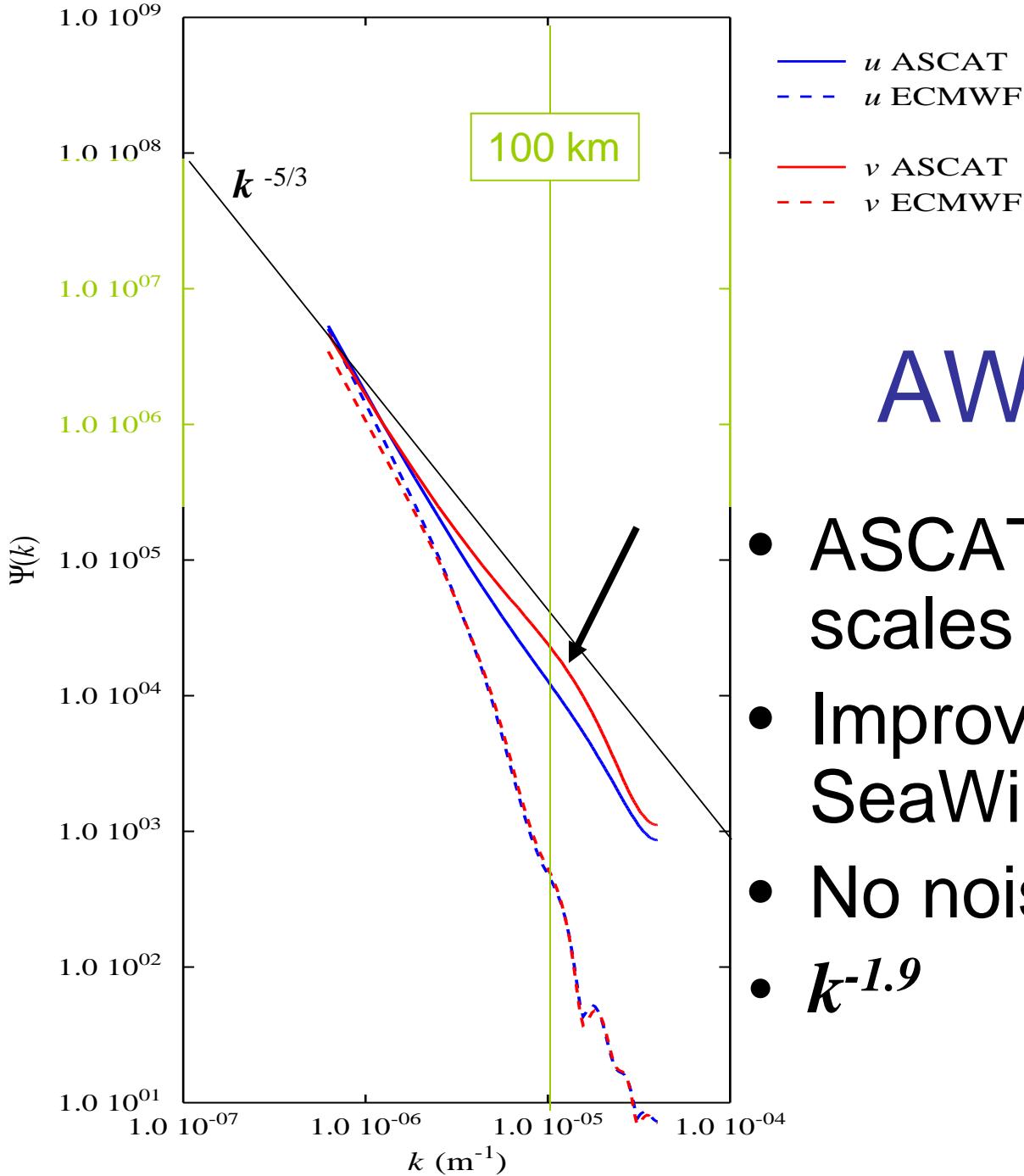
Portabella & Stoffelen, 2006

Accuray on 50-km WVC scale

- Triple collocation analysis of buoy, scatterometer & NWP

| Vector RMS error [m/s] | Tropical TAO/PIRATA | Extratropical NDBC/MEDS/UKMO |
|---------------------------|------------------------|---------------------------------|
| Buoy | 1.5 | 1.5 |
| Scatterometer | 1.2 | 1.6 |
| ECMWF model | 2.0 | 2.1 |

Scatterometer winds provide excellent forcing
Remaining errors include representativeness



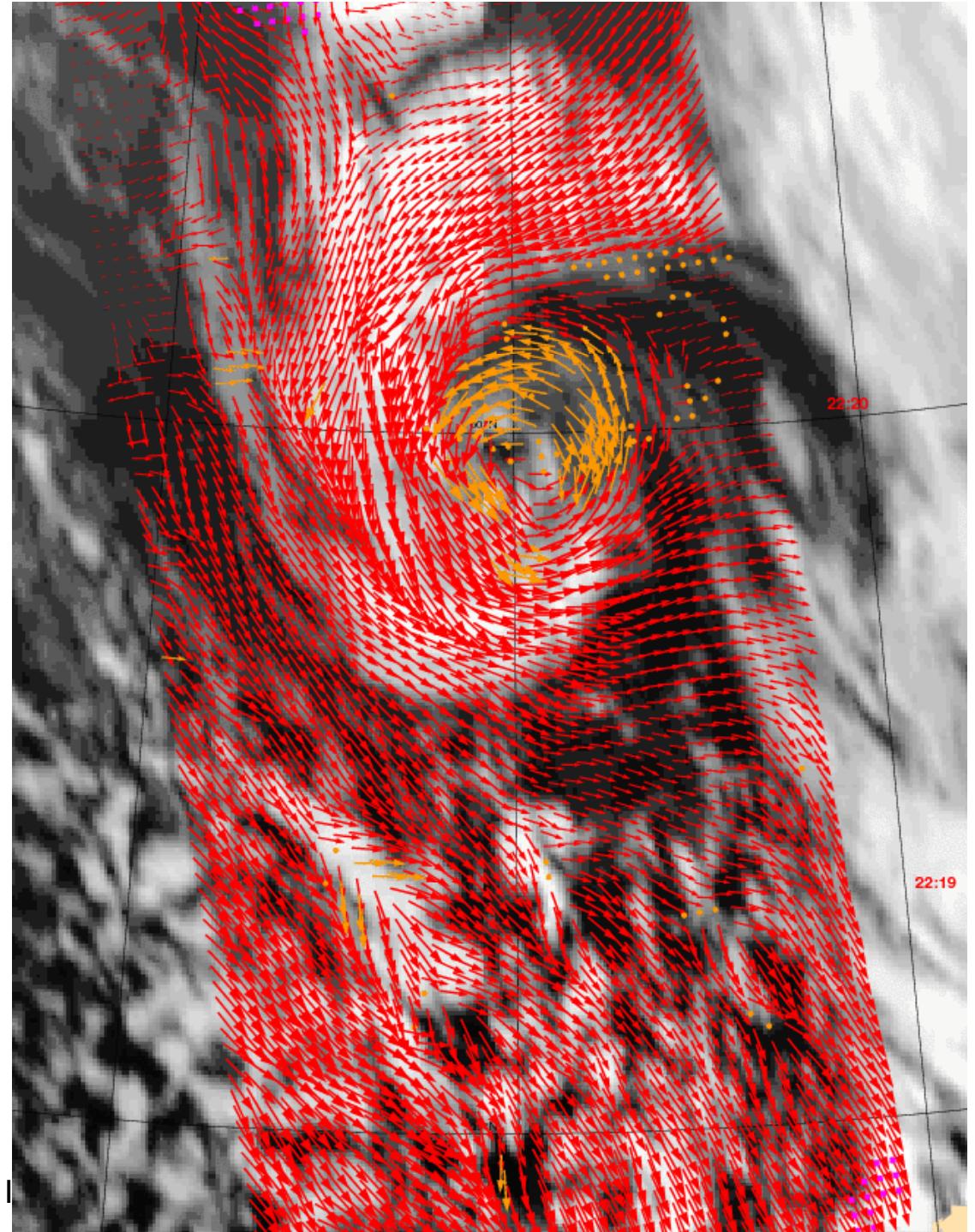
AWDP@12.5

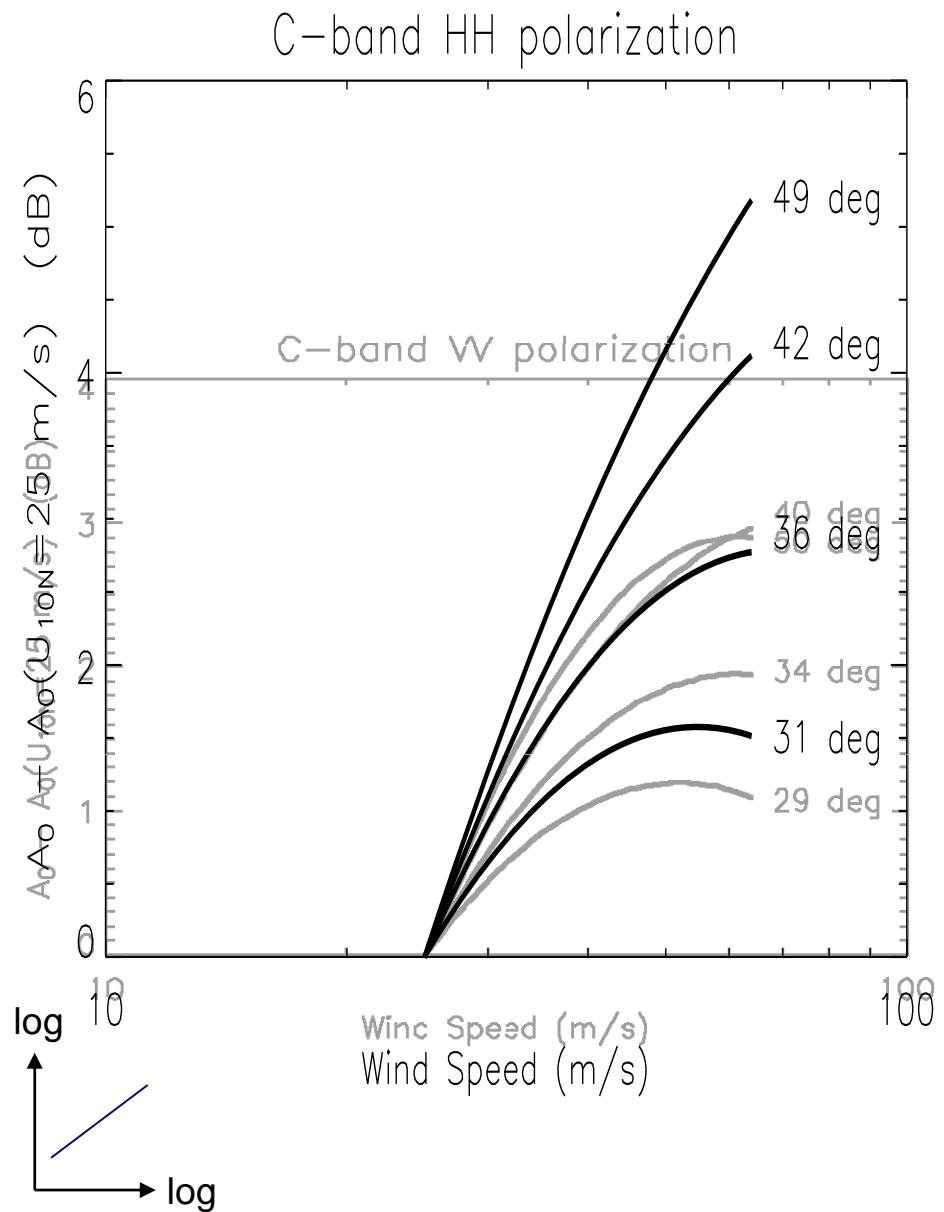
- ASCAT contains small scales down to 25 km
- Improved w.r.t. SeaWinds
- No noise floor
- $k^{-1.9}$

Mesoscales

- 12.5-km box details appear spectrally correct
- It verifies well with buoys
- It corresponds well with cloud features

www.knmi.nl/scatterometer



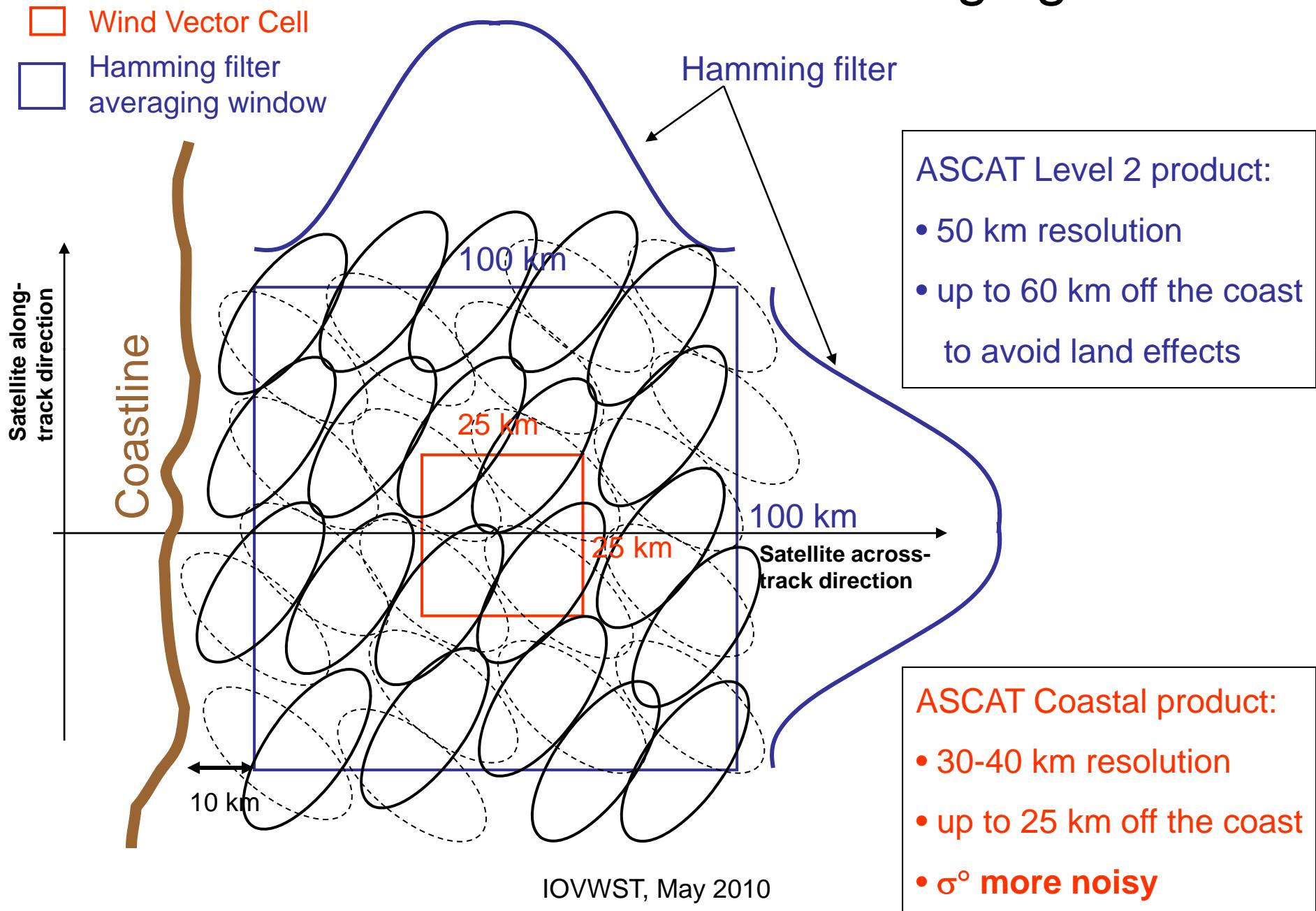


High Winds C-band Model Function

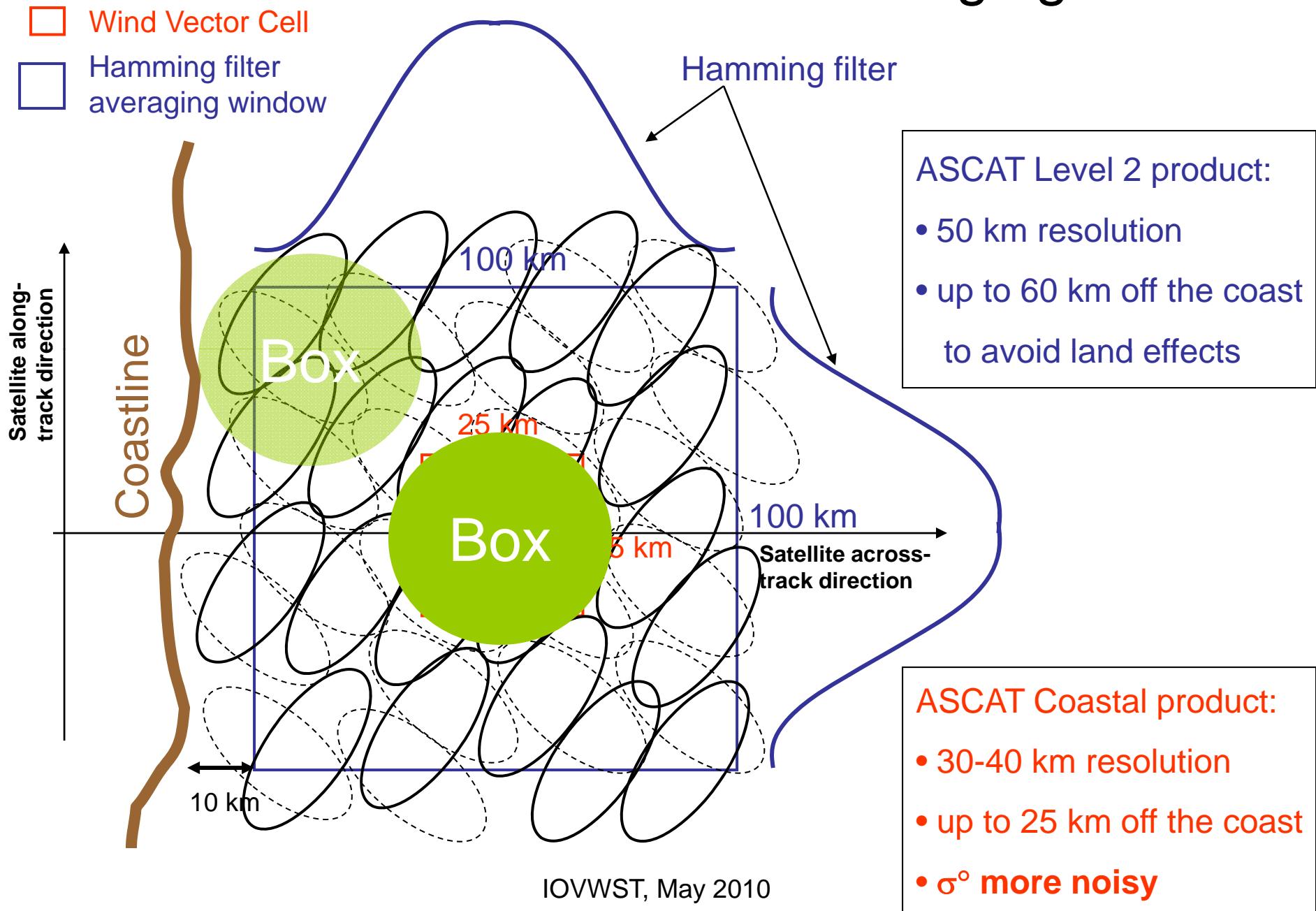
- C-band HH sensitive to high winds
- No EUM priority due to lack of high winds

Courtesy
D. Esteban
JPL, NASA

ASCAT L1 backscatter averaging

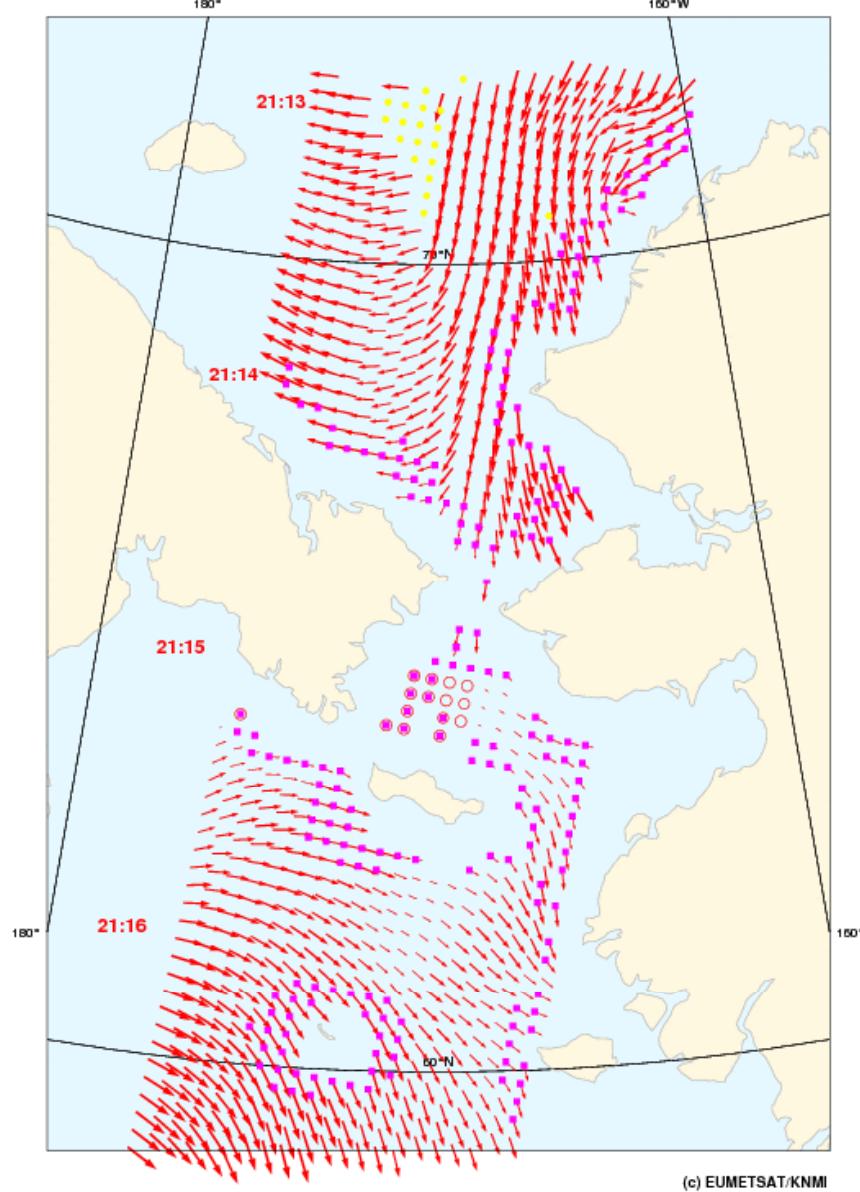


ASCAT L1 backscatter averaging

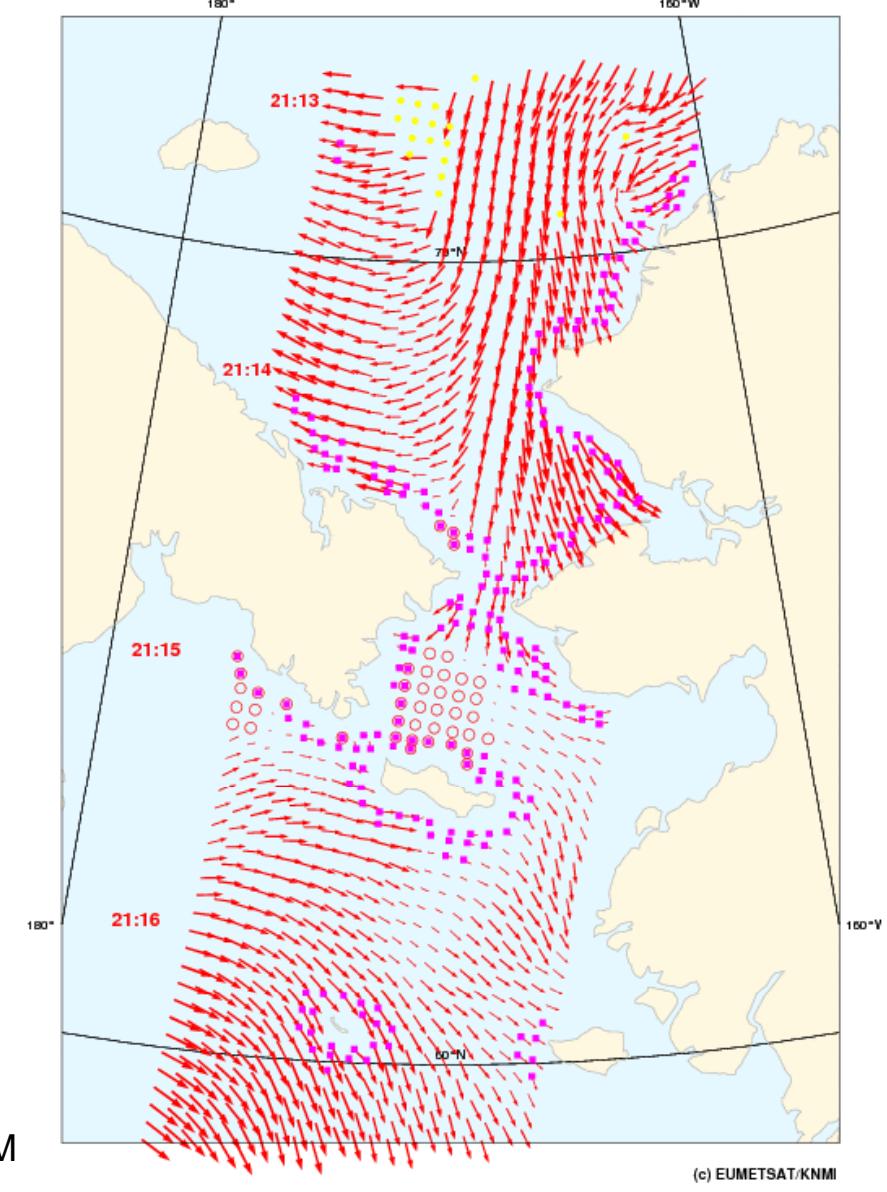


Prototype at 25 km

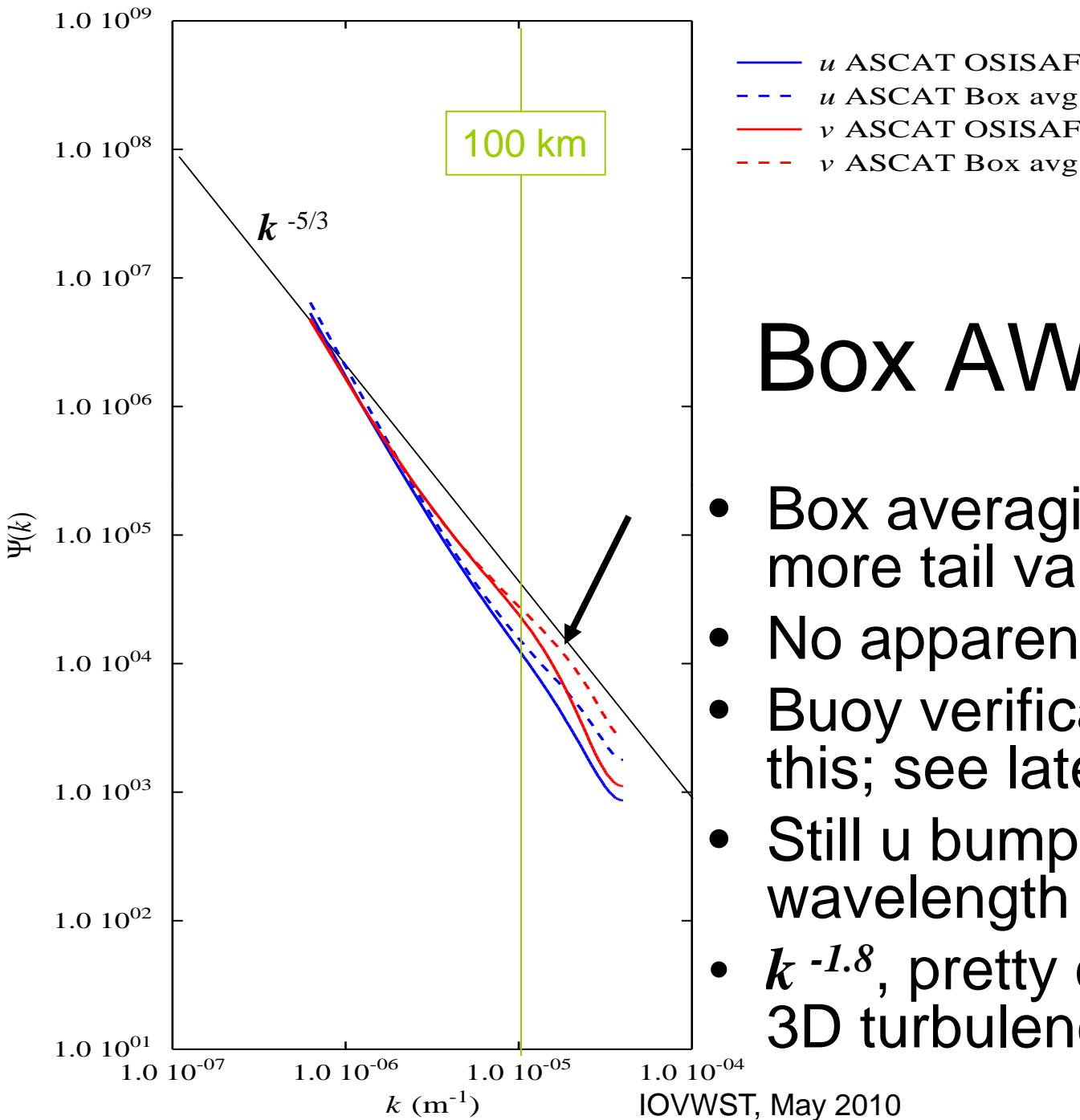
ASCAT: 20070709 21:30Z lat lon: 66.00 -170.00



ASCAT: 20070709 21:30Z lat lon: 66.00 -170.00

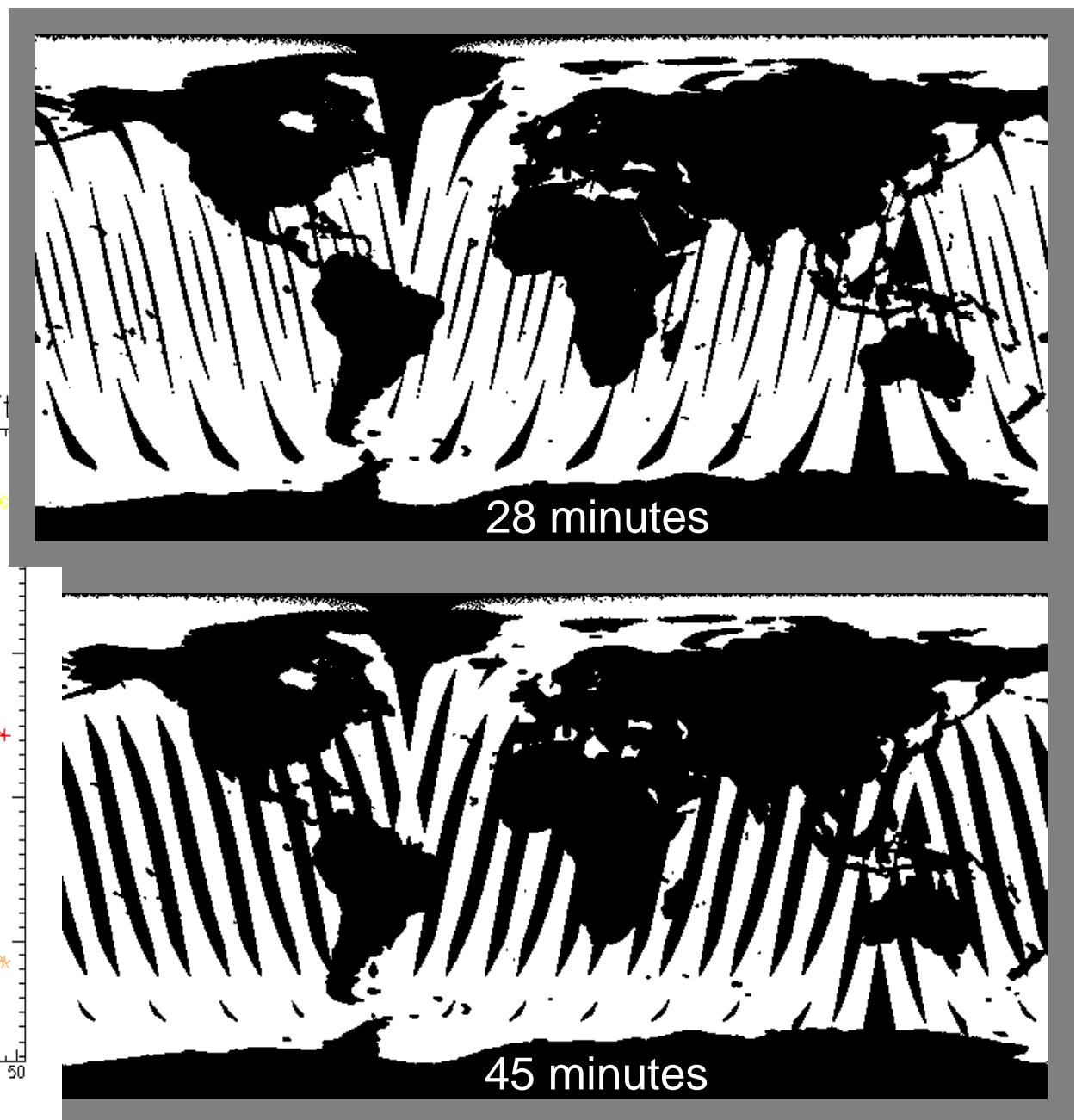
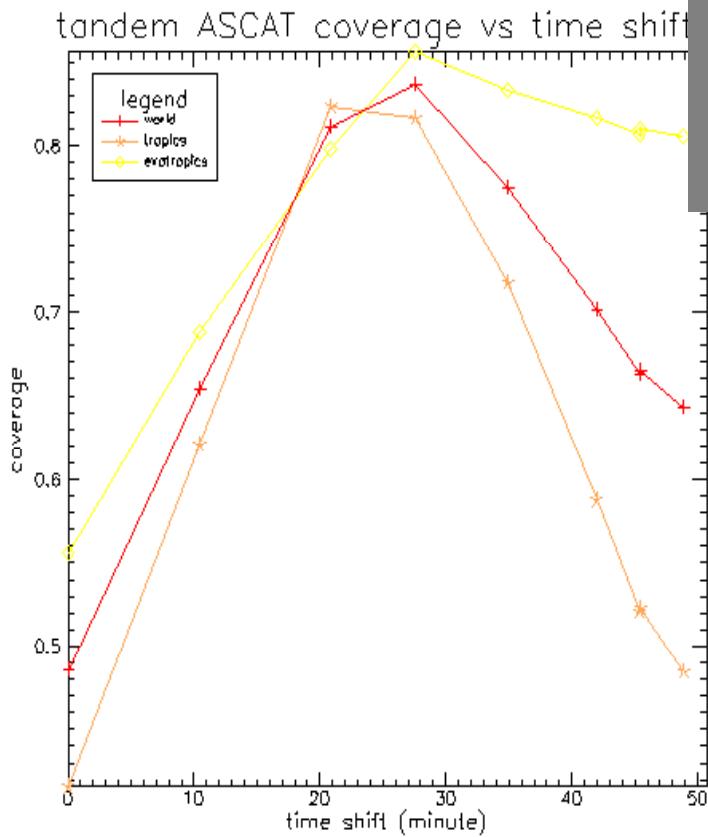


NWP
SAF



KNMI ASCAT on MetOp Phasing Study

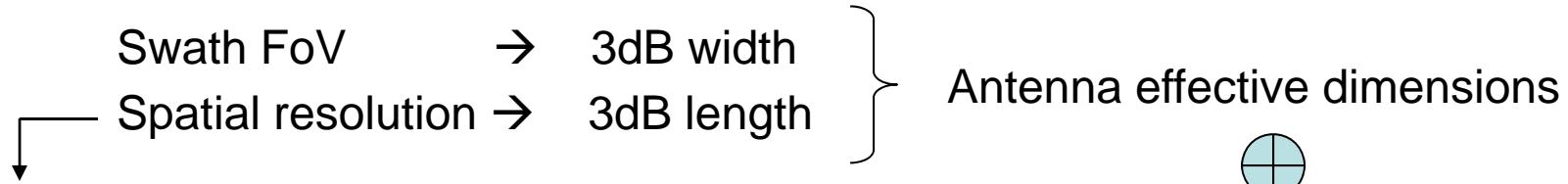
- 28 minutes clearly optimal
- No gain in tropics at 50 minutes



Antenna assembly

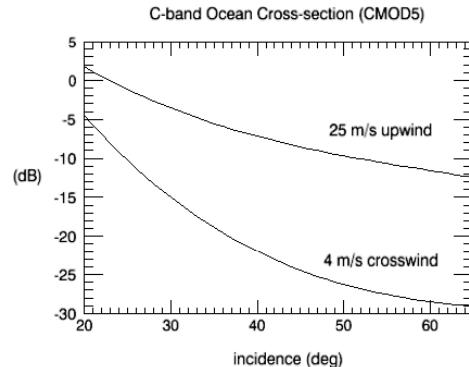
C-band, VV polarization (extension to dual HH polarization an option)

Swath FoV → 3dB width
 Spatial resolution → 3dB length } Antenna effective dimensions



A bracket groups the two statements above it, indicating they both contribute to defining the "Antenna effective dimensions". An arrow points from the bracket to a circular icon divided into four quadrants, representing the antenna's effective aperture.

20% better than
 ASCAT on MetOp
 (from 20 to 16 km)

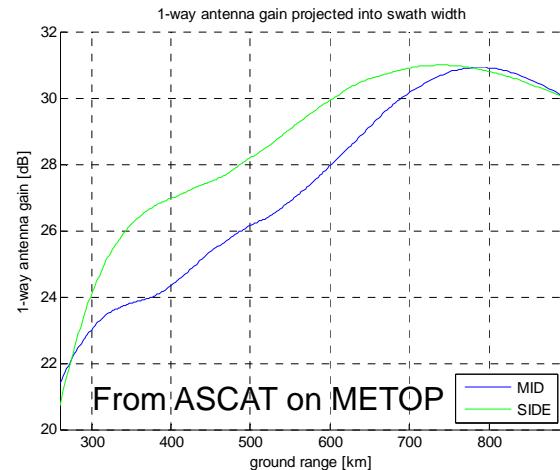


Dynamic range

$$SNR = \frac{\frac{\lambda^2}{(4\pi)^3} \left(\frac{G_{TX} G_{RX}}{R^4 \cdot L_{prop}} \right) \sigma^0 A_{look}}{k_B (T_0 + T_{eq})} \frac{B_{look}}$$

[SNR is determined by Pt and chirp bandwidth]

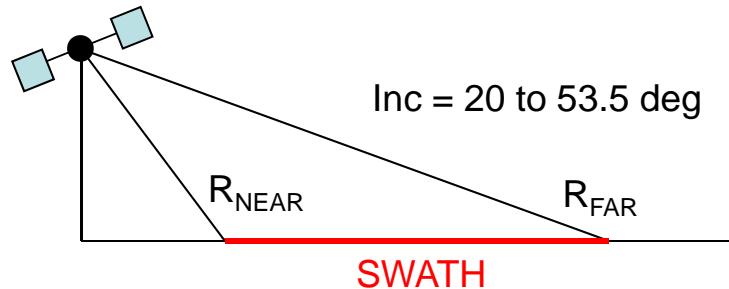
Beam shaping in elevation



Slotted waveguide radiators:
 to compensate for larger slant range
 across swath (~10 dB)

Radar PRF

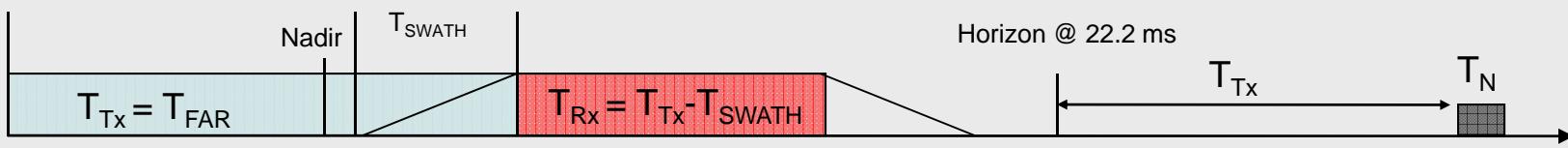
Limited by swath extent: two different strategies



| T_{SWATH} | MID | SIDE |
|-------------|--------|---------|
| T_{NEAR} | 5.7 ms | 8.4 ms |
| T_{FAR} | 6.0 ms | 10.5 ms |

A) Long pulse ($T_{TX} \gg t_{SWATH}$)

$$PRF = 1/(T_{HOR} + T_{Tx} + T_N) = 29.4 \text{ Hz (30\%DC)}$$



B) Short pulse ($T_{TX} \ll t_{SWATH}$)

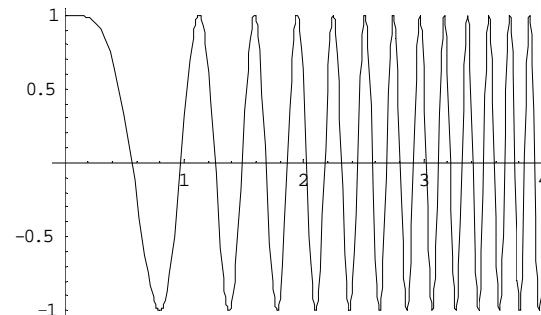
$$PRF = 1/(T_{FAR} + T_{Tx}) = 230 \text{ Hz (7\%DC)}$$



2) Radar waveform

LFM chirp for range resolution

$$\text{Chirp} \sim \exp[i(\mu/2)t^2]$$



$$(\mu = \text{chirp rate} \approx B_{\text{Tx}}/T_{\text{Tx}})$$

Deramping $\sim \exp[-i(\mu/2)t^2] \exp[i f_D t + i(\mu/2)(t-t_r)^2] = \exp[i(f_D + i\mu t_r)t]$



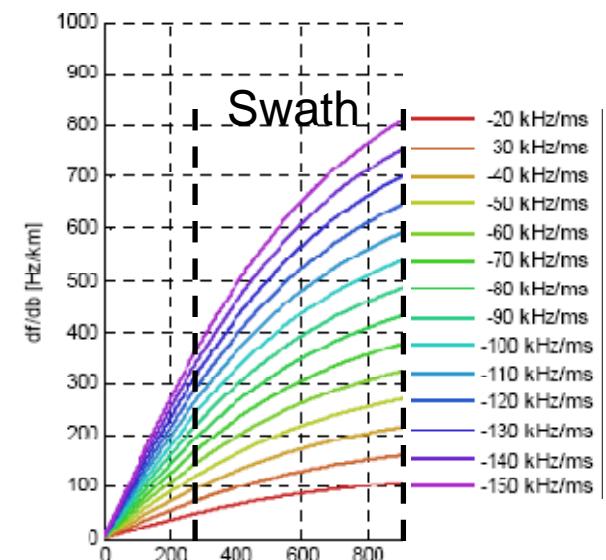
$$\text{Echo bandwidth } B_{\text{echo}} \approx \mu(t_{\text{FAR}} - t_{\text{NEAR}}) + \Delta f_D$$

$$\text{Detection bandwidth } B_{\text{detection}} \approx 1/T_{\text{RX}} = B_{\text{look}}$$

Resolved look area:

$$A_{\text{look}} = 16 \text{ km} \times \boxed{B_{\text{look}}/[2(\mu/c)\sin(\text{inc})]}$$

Inversely proportional to chirp rate, but so is SNR!
IOVWST, May 2010



$$dB_{\text{echo}}/dx \approx 2(\mu/c)\sin(\text{inc})$$

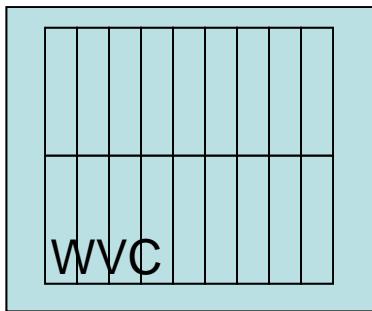
Radiometric resolution

Received signal = backscatter + speckle + emission

$$K_p^2 = \frac{\text{var}\{\sigma^0\}}{\langle\sigma^0\rangle^2} = \frac{1}{N_{\text{looks}}} \left(1 + \frac{1}{SNR}\right)^2 + \frac{1}{N_{\text{noise}}} \left(\frac{1}{SNR}\right)^2$$

1) Accumulate independent looks to reduce speckle

$$N_{\text{looks}} = N_{\text{az}} N_{\text{el}}$$



Independent looks

$$N_{\text{az}} = (\text{PRF}/v_{\text{ground}}) L_{\text{WVC}}$$

Maximum PRF
(compatible with unambiguous range)

$$N_{\text{el}} = [2(\mu/c)\sin(\text{inc})/B_{\text{look}}] L_{\text{WVC}}$$

Maximum μ
(compatible with SNR >-1.5dB)

$$\text{SNR} \propto P_t \sigma^0 / \mu \sin(\text{inc})$$

Minimum P_t
(compatible with K_p requirements)

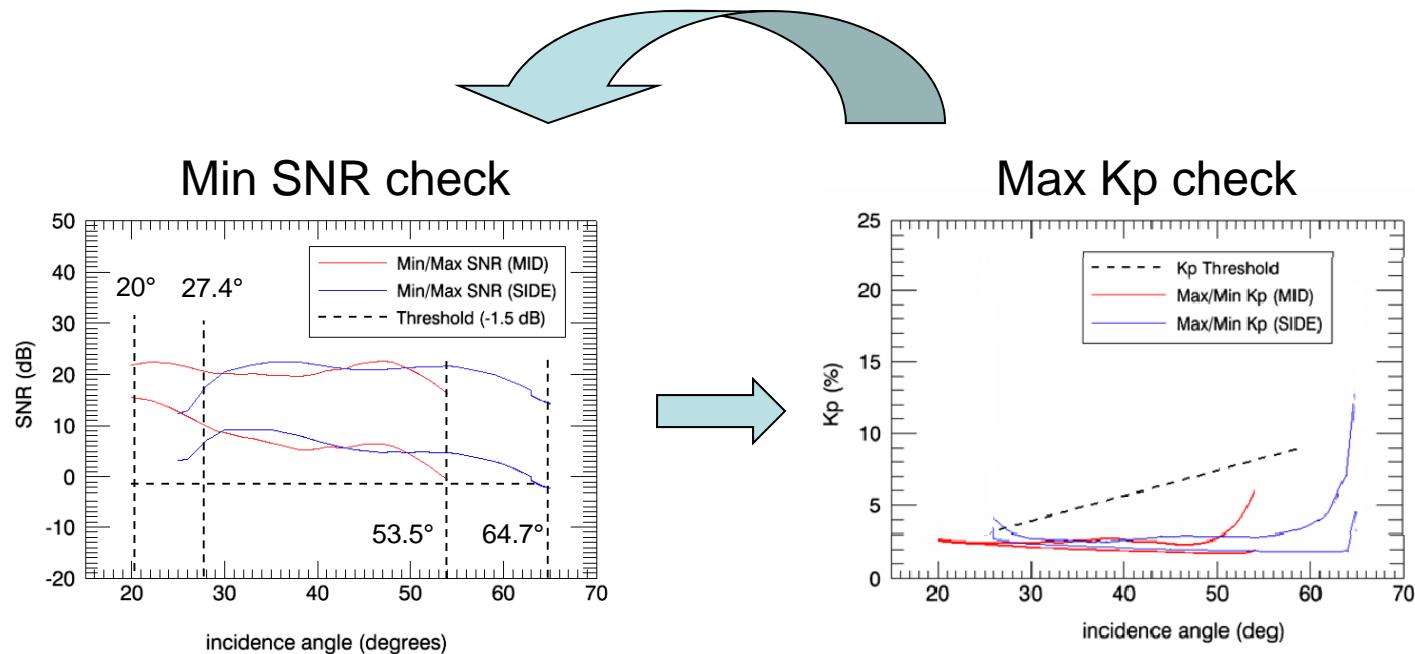
ITERATE

2) Noise (emission) estimation and subtraction

$$N_{\text{noise}} = N_{\text{az}} B_{\text{echo}} T_N$$

Where $B_{\text{echo}} = f_s/2$ sets the sampling frequency

Trade-offs to optimize K_p via chirp rate and total power (antenna pattern)



Non-compliance leads to
increments in peak power

(and/or antenna pattern accommodation?)

Non-compliance leads to
increments in chirp rate

Compliant SCA configurations enter the wind performance study

Complete SCA configuration

1) Antenna assembly
- total power & pattern

2) Radar waveform
- PRF, chirp rate & noise

Orbital model

Pseudo Level 1B file

| Row/Col | Lat/Lon | | Satellite position and velocity | | | | | | # Views | |
|---------|---------|------|---------------------------------|-------|---------|-------|-------|-------|---------|---|
| 0 | 0 | 6.78 | 1.53 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 3 |
| 0 | 0.00 | a | 135.00 | 28.51 | 3046.00 | 6.90 | VV | | | |
| 1 | 0.00 | a | 90.00 | 20.40 | 2514.00 | 23.71 | VV | | | |
| 2 | 0.00 | a | 45.00 | 28.51 | 3046.00 | 6.90 | VV | | | |
| 0 | 1 | 7.58 | 4.28 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 3 |
| 0 | 0.00 | a | 135.00 | 28.51 | 3046.00 | 6.90 | VV | | | |
| 1 | 0.00 | a | 90.00 | 21.29 | 2632.00 | 23.23 | VV | | | |
| 2 | 0.00 | a | 45.00 | 28.51 | 3046.00 | 6.90 | VV | | | |
| 0 | 2 | 8.03 | 3.31 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 3 |
| 0 | 0.00 | a | 135.00 | 29.69 | 3194.00 | 7.31 | VV | | | |
| 1 | 0.00 | a | 90.00 | 22.16 | 2750.00 | 22.79 | VV | | | |
| 2 | 0.00 | a | 45.00 | 29.69 | 3194.00 | 7.31 | VV | | | |
| 0 | 3 | 8.47 | 2.34 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 3 |
| 0 | 0.00 | a | 135.00 | 30.85 | 3341.00 | 7.75 | VV | | | |
| 1 | 0.00 | a | 90.00 | 23.03 | 2867.00 | 22.39 | VV | | | |
| 2 | 0.00 | a | 45.00 | 30.85 | 3341.00 | 7.75 | VV | | | |

View counter

WVC Node

Views

Azimuth Incidence # Looks 1/NESZ Polarization

NESZ (Noise Equivalent Sigma Zero):

$$NESZ = \frac{\sigma^0}{SNR} = \frac{k_B(T_0 + T_{eq})}{\lambda^2} \frac{B_{look}}{(4\pi)^3 \left(\frac{P_t G_{TX} G_{RX}}{R^4 \cdot L_{prop}} \right)} A_{look}$$